NATIONAL BUILDING CODE

TECHNICAL STANDARD OF BUILDING E.030

"EARTHQUAKE-RESISTANT DESIGN"

TECHNICAL BUILDING STANDARD E.030

PERMANENT TECHNICAL COMMITTEE NTE E-030 EARTHQUAKE RESISTANT DESIGN

President : Dr. Javier Piqué del Pozo Vice president : MSc Eng. Alejandro Muñoz Peláez Technical Secretary: SENCICO

CONTENTS

Pág.

CHAPTER 1 GENERAL

1.1 Objective

- a) This Technical Standard stablish the minimum conditions for the Earthquake-Resistant Design of the buildings.
- b) Until specific national standards for structures such as reservoirs, tanks, silos, bridges, transmission towers, docks, hydraulic structures, tunnels, and all those whose seismic behavior differs from that of buildings are available, the values of Z and S from Chapter II must be used, amplified according to the importance of the structure, considering international practice.

1.2 Scope

- a) It is mandatory at the national level.
- b) It applies to the design of all new buildings, the strengthening of existing ones, and the repair of structures that are damaged by seismic action.

1.3 Philosophy and Principles of Earthquake-Resistant Design

The philosophy of earthquake-resistant design consists in:

- a) Avoid human losses.
- b) Ensure the continuity of the basic services.
- c) Minimize property damages.

It is well known that to give complete protection against every earthquake is not technically or economically feasible for most buildings. In accordance with such philosophy, it has been established in this standard the following design principles:

- a) The structure must not collapse or cause serious damage to people, although could have important damages, due to severe seismic movements that may occur in site.
- b) The structure should endure ground movements qualified as moderate for the project site; the structure could experience repairable damages within the acceptable limits.
- c) Essential buildings, defined in Table N° 5, will have special considerations oriented to achieve that the building remains operating after a severe earthquake.

1.4 Approval of Other Structural Systems

The use of structural systems different from those indicated in 3.3 is approved by the Ministry of Housing, Construction, and Sanitation through a study that demonstrates that the proposed alternative produces adequate results in terms of stiffness, seismic resistance, and ductility.

1.5 Other Prevention Measures

In addition to what is indicated in this standard, measures must be taken to prevent disasters that may occur as a result of seismic movement, suc as tsunamis, fire, the release of hazardous materials, massive landslides, or others.

1.6 Nomenclature

For the purposes of this technical standard, the following nomenclatures are considered:

- *C* Seismic amplification coefficient.
- C_T Coefficient to estimate the predominant period of a building.
- D_i Lateral displacement of the center of mass of level i in the pure translation (restricting the turns in plant) due to the forces *fi*.
- *eⁱ* Accidental eccentricity of level *i*.
- *Fⁱ* Horizontal seismic force of level *i*.
- *g* Gravity acceleration.
- h_i Height of story *i* with respect to ground level.
- *hei* Height of story *i.*
- *hⁿ* Total height of building in meters.
- *Mti* Accidental torsion moment in story *i.*
- *m* Number of modes used in modal combination.
- *n* Number of stories in the building.
- *P* Total weight of the building.
- *Pⁱ* Weight of story *i.*
- *R* Reduction coefficient of seismic solicitations.
- *r* Maximum elastic structural response expected.
- *rⁱ* Maximum elastic responses corresponding to mode *i.*
- Soil amplification factor.
- *S^a* Spectrum of pseudo accelerations.
- *T* Fundamental period of the structure for static analysis or period of a mode in dynamic analysis.
- *T^P* Period that defines the spectral platform for seismic amplification coefficient.
- *T^L* Period that defines the beginning of seismic amplification coefficient zone with constant displacement.
- *U* Use and importance factor.
- *V* Seismic base shear of the structure.
- *Z* Zone factor.
- *R⁰* Basic coefficient of reduction of seismic forces.
- *I^a* Factor of irregularity in elevation.
- *I^p* Factor of irregularity in floor.
- f_i Lateral force of level i .
- \bar{V}_s Average velocity of propagation of shear waves.
- \bar{N}_{60} Weighted average of the standard penetration tests.
- $\bar{\mathcal{S}}_u$ Weighted average of shear strength in undrained condition.

1.7 Earthquake-resistant Structural Conception

Must be taken into account the importance of the following aspects:

- Symmetry, both in the distribution of masses and rigidities.
- Minimum weight, especially in high floors.
- Proper use and selection of construction materials.
- Adequate resistance against lateral loads.
- Structural continuity, both in plant and elevation.
- Ductility, understood as the structure deformation capacity beyond the elastic range.
- Limited lateral deformation.
- Inclusion of resistance successive lines (structural redundancy)
- Consideration of local conditions.
- Good constructive practice and rigorous structural supervision.

1.8 General Considerations

Every building and its parts will be designed and built to resist the required seismic demands in the standard, following the specifications of the pertinent codes to the used materials.

Is not necessary to consider simultaneously wind and earthquake effects.

Must be considered the possible effect of partition walls, parapets and other attached elements in the structure seismic behavior. The analysis, the reinforcement details and the anchorage must be done according this consideration.

In accordance with the earthquake-resistant design principles of the item 1.3, it is accepted that the buildings may have inelastic incursions against severe seismic demands. Thus, the design seismic forces are a fraction of the elastic maximum seismic demand.

1.9 Project Presentation

The plans, descriptive memory and technical specifications of the structural project, must be signed by the college civil engineer responsible of the design, who will be the only one authorized to approve any modification.

The plans of the structural project must include the following information.

- a) Earthquake-resistant structural system.
- b) Fundamental period of vibration in both principal directions.
- c) Parameters to define the seismic force or the design specter.
- d) Shear force in the base used for the design, in both directions.
- e) Maximum displacement of the last floor and the maximum relative displacement of mezzanine.
- f) The location of the accelerometers stations, if needed according the Chapter 9.

CHAPTER 2 SEISMIC HAZARD

2.1 Seismic Zones

Peru is divided in four zones, as shown in Figure N°1. The zonation is based on the spatial distribution, source parameters and attenuation of earthquakes, as well as the neotectonic information. Appendix N°02 displays the list of provinces and districs and their corresponding seismic zones.

SEISMIC ZONES

FIGURE N° 1

Every zone is correlated to a site coefficient *Z* as shown in Table N°1. This coefficient represents the peak ground acceleration (PGA) for stiff soil type with a probability of exceedance of 10 percent in 50 years. The PGA is expressed in gravity or *g*.

2.2 Seismic Microzonation and Site Studies

2.2.1 Seismic Microzonation

It requires multi-disciplinary approaches in order to assess the earthquakeinduced phenomena such as soil liquefaction, landslides, tsunamis, and others. These studies contribute to estimate the response of soil layers under earthquake excitations and thus to explain the variation of earthquake characteristics on the ground surface; as well as establish the design requirements for the construction of new buildings and certain types of structures.

The results obtained from microzonation studies are very useful in the following cases:

- Places for urban development.

- Reconstruction of damaged zones.

2.2.2 Specific Site Response Analyses

These analyses are similar to the microzonation study, but not at all in its extension. These studies are only applied to the investigated area and provide information about the variation of earthquake characteristics on the ground surface. The main objective is determined the seismic design parameters.

The site surveys must conduct at heavy industrial sectors, industries that generate explosive, flammable and polluting materials.

The seismic design parameters must not be lower than the coefficients established by this code.

2.3 Getechnical Characterization

2.3.1 Site Profiles

For this building code, site profiles classify according to the average shear wave velocity ($\bar{V}_{\rm s}$). For cases where measured $\bar{V}_{\rm s}$ data is not available, site profiles can also classify in terms of the average standard penetration resistance \bar{N}_{60} for cohesionless soils estimated from the Standard Penetration Test (SPT), and the average undrained shear strength (\bar{S}_u) for cohesive soils. These properties are determined of the top 30 m of the

subsurface profile extending from the base of the foundation, as indicated in the section 2.3.2.

For cohesionless soils, \bar{N}_{60} is calculated using only the cohesionless soil layers. In terms of cohesive soils, the undrained shear strength \bar{S}_u is computed using the average result from cohesive soil layers.

The methodology explained above is also applicable for heterogeneous soils (cohesionless and cohesive). If \bar{N}_{60} for cohesionless soils and \bar{S}_u for cohesive soils criteria differ, the site must be assigned to the category with the softer soil.

The types of site profiles are five:

a. Site Class *S0***: Hard Rock**

This site corresponds to intact bedrock with shear wave velocity $\bar{V}_{\scriptscriptstyle{S}}$ greater than 1500 m/s. This category must be supported by shear wave velocity measurement either on site or on profiles of the same rock type in the same formation with an equal or greater degree of weathering and fracturing. Where hard rock conditions are known to be continuous to a depth of 30 m, surficial shear wave velocity measurements are permitted to be extrapolated to assess $\bar{\mathit{V}}_{\!s}$.

b. Site Class *S1***: Rock or Very Dense Soils**

This site corresponds to rocks with different degrees of fracturing, competent rocks, very dense soils with shear wave velocities \bar{V}_{s} ranging from 500 to 1500 m/s, including when the foundation is constructed on:

- Fractured rock, with an unconfined compression strength qu greater or equal that 500 kPa (5 kg/cm²).
- Very dense sand or dense sandy gravel, with \bar{N}_{60} greater than 50.
- Very stiff clay (with a thickness larger than 20 m), with an undrained shear strength \bar{S}_u greater than 100 kPa (1 kg/cm²) and its mechanical properties are increasing gradually with the depth.

c. Site Class *S2***: Stiff Soils**

This site corresponds to stiff soils, with shear wave velocities \bar{V}_{s} ranging from 180 to 500 m/s, including when the foundation is constructed on:

- Dense sand, medium to coarse, or sandy gravel, medium, with SPT resistance values \bar{N}_{60} within 15 and 50.
- Stiff cohesive soil, with an undrained shear strength \bar{S}_u within 50 kPa (0.5 kg/cm^2) and 100 kPa (1 kg/cm^2) , and its mechanical properties are increasing gradually with the depth.

d. Site Class *S3***: Soft Soils**

This site corresponds to soft soils, with shear wave velocities $\bar{V}_{\rm s}$ less than or equal to 180 m/s, including when the foundation is constructed on:

- Fine to medium sand, or sandy gravel, with SPT resistance values \bar{N}_{60} less than 15.
- Soft cohesive soil, with an undrained shear strength \bar{S}_u within 25 kPa $(0,25 \text{ kg/cm}^2)$ and 50 kPa $(0,5 \text{ kg/cm}^2)$, and its mechanical properties are increasing gradually with the depth.
- Sites that not correspond to S_4 , with a total thickness greater than 3 m and having the following characteristics: plasticity index P greater than

20, moisture content ω greater than 40%, and undrained shear strength \bar{S}_u less than 25 kPa.

e. Site Class *S4***: Special Soils**

This site corresponds to very soft soils as well as the places where geologic and/or topographic conditions are particularly unfavorable, so a site response analysis must be performed. A site qualifies under the criteria for Site Class S_4 as long as the results of the geotechnical analysis indicates that.

Table N°2 shows the site classification for the different types of soil profiles:

2.3.2 Definitions of Site Class Parameters

The definitions presented in this section must apply to the upper 30 m of the site profile, extending from the base of the foundation. The symbol i refers to n distinct layers in the top 30 m, where some of the n layers are cohesive and others are not, m is the number of cohesionless layers and k is the number of cohesive layers.

a. Average Shear Wave Velocity, \overline{V}_s

The average shear wave velocity must be determined in accordance with the following formula:

$$
\overline{V}_s = \frac{\sum_{i=1}^n d_i}{\sum_{i=1}^n \left(\frac{d_i}{V_{si}}\right)}
$$

Where *dⁱ* is the thickness of each one of the *n* layers and *Vsi* is the shear wave velocity (m/s).

b. Average Standard Penetration Resistance, \bar{N}_{60}

 \overline{N}_{60} must only be determined for cohesionless soil layers of the upper 30 m of the site profile, in accordance with the following formula:

$$
\overline{N}_{60} = \frac{\sum_{i=1}^{m} d_i}{\sum_{i=1}^{m} \left(\frac{d_i}{N_{60i}}\right)}
$$

Where d_i is the thickness of the m cohesionless soil layers, and N_{60i} is the corrected SPT value.

c. Average Undrained Shear Strength, \overline{S}_u

 $\bar{\mathit{S}}_u$ must only be determined for cohesive soil layers of the top 30 m of the site profile, in accordance with the following formula:

$$
\bar{s}_u = \frac{\sum_{i=1}^k d_i}{\sum_{i=1}^k \left(\frac{d_i}{s_{ui}}\right)}
$$

Where d_i is the thickness of the k cohesive soil layers, and S_{ui} is the undrained shear strength (kPa).

Other Important Considerations:

In the case that geotechnical studies are not mandatory or the soil properties are unknown for the upper 30 m, the engineer can assume appropriate site class parameters based on his experience and knowledge.

For deep foundation systems like piles, the site profile is determined of the upper 30 m, extending from the pile top.

2.4 Site Coefficients (*S***,** *T^P* **y** *TL***)**

The site profile that describes the local site conditions is determined in accordance of the soil amplification factor S and the period site coefficients T_P and T_L given in Tables N°3 and N°4, respectively.

2.5 Seismic Amplification Factor (C)

According to the local site conditions, the site amplification factor (C) is determined in accordance with the following equations:

$$
T < T_P
$$
 $C = 2.5$

$$
T_P < T < T_L \qquad \qquad C = 2.5 \cdot \left(\frac{T_P}{T}\right)
$$

$$
T > T_L \qquad \qquad C = 2.5 \cdot \left(\frac{T_P \cdot T_L}{T^2}\right)
$$

T is the period according to items 4.5.4 and 4.6.1.

This coefficient means the amplification factor due to the acceleration of the structure with respect to the ground acceleration.

CHAPTER 3 CATEGORY, STRUCTURAL SYSTEM AND BUILDING REGULARITY

3.1 Building Category y Importance Factor (*U***)**

Each Structure shall be classified according to the category indicated in Table N° 5. The importance or usage factor (U) , defined in Table N° 5 will be used according to the realized classification. For buildings with base isolation systems may be considered $U = 1$.

the responsible entity can decide whether or not to use base isolation systems. If base isolation system is not used in seismic zones 1 and 2, the value of U shall be at least 1.5.

Note 2: In these buildings must be provided adequate strength and stiffness for lateral actions, at the discretion of the designer.

3.2 Structural Systems

3.2.1 Reinforced Concrete Structures

All reinforced concrete elements that make up the earthquake resistant structural system shall satisfy the provisions of Chapter 21 "Special provisions for seismic design" of Technical Standard E.060 Reinforced Concrete of the RNE.

Moment Frames: At least 80% of the shear force at the base acts on the columns of the frames. In the case of structural walls, they shall be designed to withstand a fraction of the total seismic action in accordance with their stiffness.

Structural Walls: System in which seismic resistance is predominantly given by structural walls on which at least 70% of the shear force at the base acts.

Dual: Seismic actions are resisted by a combination of frames and structural walls. The shear force taken by the walls is between 20% and 70% of the shear at the base of the building. Frames shall be designed to withstand at least 30% of the shear force at the base.

Buildings of Limited Ductility Walls (EMDL): Buildings characterized by having a structural system where seismic and gravity load resistance is given by reinforced concrete walls of reduced thickness, in which confined ends are dispensed and the vertical reinforcement is arranged in a single layer.

With this system, a maximum of eight floors can be built.

3.2.2 Steel Structures

The systems listed below are part of the Earthquake Resistant Structural System.

Special Moment Frames (SMF)

These frames must provide a significant inelastic deformation capacity through the yielding by bending of beams and limited yielding in the panel zones of columns. Columns shall be designed to have a greater strength than the beams when they reach the deformation hardening zone.

Intermediate Moment Frames (IMF)

These frames must provide limited inelastic deformation capacity in their elements and connections.

Ordinary Moment Frames (OMF)

These frames must provide a minimum inelastic deformation capacity in their elements and connections.

Special Concentrically Braced Frames (SCBF)

These frames must provide a significant inelastic deformation capacity through the post-buckling strength in braces in compression and creep in braces in tension.

Ordinary Concentrically Braced Frames (OCBF)

These frames must provide limited inelastic deformation capacity in their elements and connections.

Eccentrically Braced Frame (EBF)

These frames must provide a significant inelastic deformation capacity mainly due to the yielding by bending or shear in the zone between braces.

3.2.3 Masonry structures

Buildings whose earthquake resistant elements are walls based on masonry units of clay or concrete. For purposes of this Standard, no distinction is made between confined or reinforced masonry structures.

3.2.4 Wooden structures

In this group are considered buildings whose resistant elements are mainly based on wood. Truss systems and braced structures type post and beam are included.

3.2.5 Earth structures

Buildings whose walls are made with units of earth masonry or in-situ rammed earth.

3.3 Category and structural systems

According to the category of a building and the zone where it is located, it must be projected using the structural system indicated in Table N ° 6 and following the irregularity restrictions of Table N ° 10.

(*) For buildings with lightweight roofing, any structural system can be used.

(**) For small rural constructions, such as schools and medical posts, traditional materials may be used following the recommendations of the standards for such materials.

3.4 Structural Systems and Basic Coefficient of Reduction of Seismic Forces (*R0***)**

Structural systems will be classified according to used materials and the seismic-resistant structural system in each direction of analysis, as indicated in Table No. 7.

When, in the direction of analysis, the building presents more than one structural system, the lowest coefficient *R⁰* will be taken.

(*) These coefficients will only apply to structures in which the vertical and horizontal elements allow dissipation of the energy while maintaining the stability of the structure. They do not apply to inverted pendulum structures. (**) For allowable stress design.

For earth constructions, refer to the RNE Standard E.080 "Adobe". This type of constructions is not recommended in S_3 soils, nor S_4 soils.

3.5 Structural Regularity

Structures should be classified as regular or irregular for the following purposes:

- Satisfy restrictions of Table No. 10.
- Establish procedures for analysis.
- Determine the R coefficient of reduction of seismic forces.

Regular Structures are those that in their resistant configuration to lateral loads, do not present the irregularities indicated in Tables N ° 8 and Nº 9.

In these cases, the factor I_a or I_p will be equal to 1,0.

Irregular Structures are those that present one or more of the irregularities indicated in Tables N ° 8 and N ° 9.

3.6 Irregularities Factors (*I^a* , *I^p* **)**

The factor I_a will be determined as the smallest of the values in Table N° 8 corresponding to the structural irregularities, in height, in the two directions of analysis. The factor *I^p* will be determined as the lowest of the values in Table Nº 9 corresponding to the structural irregularities, in plant, in the two directions of analysis.

If, when Tables No. 8 and 9 are applied, and different values of factors *I^a* o *I^p* were obtained for the two directions of analysis, the lowest value of each factor should be taken for the two directions of analysis.

3.7 Restrictions on Irregularity

3.7.1 Building Category and Irregularity

According to the building category and the area where it is located, it must be projected respecting the restrictions to the irregularity of Table N° 10.

3.7.2 Transfer Systems

The transfer systems are structures of slabs and beams that transmit forces and moments from discontinuous vertical elements to others of the lower story.

In seismic zones 4, 3 and 2 structures with transfer system are not allowed in which more than 25% of gravity loads or seismic loads at any story are supported by vertical elements that are not continuous until the foundation. This provision does not apply to the last story of buildings.

3.8 Coefficient of Reduction of Seismic Forces, *R*

The coefficient of reduction of seismic forces will be determined as the product of the coefficient R_0 determined from Table N° 7 and the factors I_a , I_p obtained from Tables Nº 8 and Nº 9.

$$
R=R_0\cdot I_a\cdot I_p
$$

3.9 Seismic Isolated Systems and Dissipation Energy Systems

Seismic isolation systems or energy dissipation systems are permitted in the building, as long as they comply the provisions of Chapter II of this Standard are complied with, and to the extent that the requirements of the following document are applicable:

"Minimum Design Loads for Building and Other Structures", ASCE/SEI 7, current edition, Structural Engineering Institute of the American Society of Civil Engineers, Reston, Virginia, USA.

The installation of seismic isolation systems or energy dissipation systems shall be subject to specialized technical supervision by a civil engineer.

CHAPTER 4 STRUCTURAL ANALYSIS

4.1 General Considerations for the Analysis

For regular structures, the analysis can be made considering that the total of the seismic force is acting independently in two predominant orthogonal directions. For irregular structures should be assumed that the seismic force is acting in the most unfavorable direction for the design.

Vertical seismic forces are considered in the design of vertical elements, in very large horizontal elements, in post-stressed and pre-stressed elements and cantilevers of a building. It is considered that the vertical seismic force is acting in the elements simultaneously with the horizontal seismic force, and the analysis is made in the most unfavorable direction.

4.2 Models for the Analysis

The model for the analysis will consider an adequate spatial distribution of masses and stiffnesses to calculate the most significant aspects of the dynamic behavior of the structure.

For purposes of this Standard, reinforced concrete and masonry structures might be analyzed considering the inertia moment of its cross-section area, ignoring cracking and reinforcement rebars.

For buildings where can be assumed that floor systems work as rigid diaphragms, a lumped-mass model with three degrees of freedom, associated to two orthogonal components for horizontal translation and one component for rotation can be used. For that case the elements deformations must be coordinated through the rigid diaphragm condition, and the plan distribution of the horizontal forces must be done as a function of the stiffness of the resistant elements.

It should be verified that the diaphragms have enough stiffness and resistance to assure the distributions mentioned above, on the contrary, their flexibility for the seismic force distribution should be taken into account.

The model should include the partition walls that are not properly separated.

For stories that do not constitute rigid diaphragms, the resistant elements will be designed for the horizontal forces that directly correspond to them.

For the buildings in which its predominant structural elements are walls, a model that takes into consideration the interaction between walls in perpendicular directions should be considered (H walls, T walls and L walls).

4.3 Weight of the Structure (*P***)**

The weight (*P*), will be calculated by adding to the permanent and total load of the structure a percentage of the live load that will be determined as following:

- a. For buildings included in categories A and B, 50% of the live load shall be taken.
- b. For buildings included in category C, 25% of the live load shall be taken
- c. For depots, 80% of the total weight storaged can be taken.
- d. For rooftops and floors 25% of the live load can be taken.
- e. For tank, silos and similar structures 100% of the load they can support shall be considered.

4.4 Seismic Analysis Procedures

It should be used one of the following procedures:

- Static analysis or equivalent static forces (item 4.5).
- Spectral modal dynamic analysis (item 4.6).

The analysis will be made considering a model with a linear-elastic behavior and with the reduced seismic forces.

Time-history dynamic analysis procedure, described in item 4.7, can be used for verification purposes, but in no case it will be mandatory as a substitute of the procedures indicated in items 4.5 and 4.6.

4.5 Static Analysis or Equivalent Static Forces

4.5.1 Overview

This method represents the seismic forces through a system of horizontal forces acting in the mass center of each story of the building.

This procedure can be used to analyzed all the structures, regular or irregular, located in seismic zone 1, structures classified as regulars according to the item 3.5 with no more than 30 m of height and structures of reinforced concrete walls, reinforced masonry walls or confined masonry walls with no more than 15 m of height, even if they are irregulars.

4.5.2 Base Shear Force

The total shear force acting in the base of the structure, corresponding to the direction considered will be determined through the following expression:

$$
V = \frac{Z \cdot U \cdot C \cdot S}{R} \cdot P
$$

The minimum value for *C*/*R* should be considered:

$$
\frac{C}{R} \geq 0, 11
$$

4.5.3 Seismic Force Distribution in Height

The horizontal seismic forces in any level *i*, corresponding to the direction considered, will be calculated through:

$$
F_i = \alpha_i \cdot V
$$

$$
\alpha_i = \frac{P_i(h_i)^k}{\sum_{j=1}^n P_j(h_j)^k}
$$

where *n* is the number of the stories of the building, *k* is an exponent related with the fundamental period of vibration of the structure (*T*), in the direction considered, which is calculated according as follows:

- a) For *T* less than of equal to 0,5 seconds: $k = 1,0$.
- b) For *T* greater than 0,5 seconds: $k = (0.75 + 0.5 \text{ T}) \le 2.0$.

4.5.4 Fundamental Period of Vibration

The fundamental period of vibration for each direction will be estimated with the following expression:

$$
T = \frac{h_n}{C_T}
$$

Where:

- $C_T = 35$ For buildings with resistant elements in the direction considered are only:
	- a) Reinforced concrete frames without shear walls.
	- b) Ductile steel frames with moment-resistant connections, without bracing.
- $C_T = 45$ For buildings with resistant elements in the direction considered are:
	- a) Reinforced concrete frames with walls in the elevator boxes and stairs.
	- b) Braced steel frames.
- $C_T = 60$ For masonry buildings and for all dual reinforced concrete buildings, with structural walls and low ductility walls.

Alternatively, it can be used the following expression:

$$
T = 2\pi \cdot \sqrt{\frac{\left(\sum_{i=1}^{n} P_i \cdot d_i^2\right)}{\left(g \cdot \sum_{i=1}^{n} f_i \cdot d_i\right)}}
$$

Where:

- *fⁱ* is the lateral force at level *i* corresponding to a distribution in height similar to the first mode in the direction of the analysis.
- *dⁱ* is the lateral displacement in the center of mass of level *i* in pure translation (restricting plan rotations) due to the forces *fi*. the displacements will be calculated assuming a linear-elastic behavior of

the structure, and for the case of reinforced concrete and masonry structures, considering cross-section areas without cracking.

When the analysis does not consider the stiffness of the non-structural elements, the fundamental period *T* should be taken as 0,85 of the obtained value with the above formula.

4.5.5 Accidental Eccentricity

For structures with rigid diaphragm, the force acting in each level (*Fi*) will be assumed to be acting in the mass center of the corresponding level, and besides the eccentricity of the structure, the effect of the accidental eccentricity should be considered (for each direction of the analysis), as is indicated as follows:

a) In the mass center of each level, in addition to the acting static lateral force, an accidental moment (*Mti*) will be applied and it will be calculated as:

$$
M_{ti} = \pm F_i \cdot e_i
$$

For each direction of analysis, the accidental eccentricity for each level (ei) will be considered as 0,05 times the building dimension in the perpendicular direction of the analysis.

b) It can be assumed that the most unfavorable conditions can be obtained considering the accidental eccentricities with the same sign for all stories. Only the increases of the horizontal forces can be considered but not the diminutions.

4.5.6 Vertical Seismic Forces

The vertical seismic force will be considered as a fraction of the weight equal to $2/3$ $Z \cdot U \cdot S$.

In very large horizontal elements, including cantilevers, a dynamic analysis with spectrums defined in item 4.6.2 will be required.

4.6 Spectral Modal Dynamic Analysis

Any structure can be designed using the dynamic analysis results by spectral modal combination as specified in this item.

4.6.1 Modes of Vibration

The modes of vibration can be determined by an analysis procedure that considers appropriately the stiffness characteristics and mass distribution of the structure.

In each direction, the modes of vibration considered are those where the sum of effective masses is at least 90 % of the total mass, but at least the first three predominant modes in the direction of the analysis should be taken into account*.*

4.6.2 Spectral Acceleration

For each horizontal direction analyzed an inelastic spectra of pseudoaccelerations defined by the following expression will be used:

$$
S_a = \frac{Z \cdot U \cdot C \cdot S}{R} \cdot g
$$

For the analysis in the vertical direction a design spectra with values equal to 2/3 of the design spectra used for the horizontal directions, considering the values of C, defined in Section 2.5, except for the very short period zone $(T < 0.2 T_p)$ in which it is considered:

$$
T < 0.2 \, T_P \quad C = 1 + 7.5 \left(\frac{T}{T_P} \right)
$$

4.6.3 Combination Criterion

Through the combination criterion indicated, the expected maximum elastic response (*r*) can be determined for the internal forces in the elements of the structure as well as for the global parameters of the structure, such as the base shear force, story shears, overturning moments, total and relative story displacements.

The expected maximum elastic response (*r*) corresponding to the total effect of different modes of vibration used (*ri*) can be determined by using the complete quadratic combination of the calculated values for each mode.

$$
r = \sqrt{\sum \sum r_i \rho_{ij} r_j}
$$

Where *r* represents the modal responses, displacements or forces. The correlation coefficients are defined by:

$$
\rho_{ij} = \frac{8\beta^2(1+\lambda)\lambda^{3/2}}{(1-\lambda^2)^2 + 4\beta^2\lambda(1+\lambda)^2} \quad \lambda = \frac{\omega_j}{\omega_i}
$$

- *β* , fraction of the critical damping, that can be assumed as a constant and equal to 0,05 for each mode
- ω_i , ω_j are the angular frequencies corresponding to the modes i, j

Alternatively, the maximum response can be estimated through the following expressions:

$$
r = 0.25 \cdot \sum_{i=1}^{m} |r_i| + 0.75 \cdot \sqrt{\sum_{i=1}^{m} r_i^2}
$$

4.6.4 Minimum Shear Force

For each direction considered in the analysis, the shear force at the base of the building cannot be less than 80 % of the calculated value according to item 4.5 for regular structures, nor less than 90 % for irregular structures.

If it is necessary to increase the shear force to fulfill the minimum requirements indicated, all other results should be scaled appropriately, except the displacements.

4.6.5 Accidental Eccentricity (Torsional Effects)

The uncertainty in the location of the mass centers for each level can be considered through the accidental eccentricity perpendicular to the earthquake direction equal to 0,05 times the dimension of the building in the perpendicular direction to the analysis direction. For each case the most unfavorable sign should be considered.

4.7 Time – History Dynamic Analysis

The time-history dynamic analysis can be used as a complementary procedure of the specified procedures in items 4.5 y 4.6.

In this analysis type, a mathematical model of the structure that considers the histerecical behavior of the elements should be used, determining the response against a set of ground accelerations through direct integration of the equilibrium equations.

4.7.1 Acceleration Records

A set of three records of ground accelerations will be used at least for the analysis, each of them will include two components in orthogonal directions.

Each set of ground accelerations will contain a pair of components of horizontal accelerations, choosen and scaled from individual events. The accelerations records will be obtained from events whose magnitudes, distance to the fault and source mechanism are consistents with the maximum earthquake considered. When the required number of appropriate records are not available, synthetic records can be used to reach the required number.

For each pair of horizontal components of the ground motion, a pseudospectral acceleration will be generated, using the square root of the sum of the squares (SRSS) of the calculated spectral values for each component separately, with 5% of damping. Both components will be scaled by the same factor, so that in the range of periods between 0,2 *T* and 1.5 *T* (with *T* as the fundamental period), the average of the spectral values SRSS obtained for every set of records will not be less than the corresponding ordinate of the design spectrum, calculated according to item 4.6.2 with $R = 1$.

For the generation of the synthetic records, C values defined in the intem 2.5 should be considered, but not for a zone with very short periods $(T < 0.2 T_P)$, where the following expression will be considered:

$$
T < 0,2 T_P
$$
 $C = 1 + 7,5 \cdot \left(\frac{T}{T_P}\right)$

4.7.2 Models for the Analysis

The spatial mass distribution of the structure should be presented correctly in the mathematical model.

The elements behavior will be modeled consistently with the laboratory test results, and it has to be taken into account the fluency, the strength degradation, the stiffness degradation, the pinching of the hysteretic curve and all the important aspects of the structural behavior shown by the tests.

The elements strength will be obtained based on the material strength expected values, hardening due to deformation and strength degradation due to the cyclic loading.

It is allowed to assume linear properties for those elements whose behavior remains in the elastic range as is shown by the analysis.

It is allowed to assume a viscous equivalent damping with a maximum value of 5 % of the critical damping, besides the dissipation due to the hysteretic behavior of the elements.

It can be assumed that the structure is perfectly fixed to the base, or alternatively, consider the flexibility of the foundations if applicable

4.7.3 Processing of the results

In case that at least seven set of ground motion records are used, the design forces, elements deformations and story drift, will be evaluated from the average of the corresponding maximum result obtained in the analysis. If the number of records used were less than seven, the design forces, the deformations and the story drift will be avaluated from the maximum values obtained in all the analysis.

The maximum story drift should not exceed 1,25 times the values indicated in Table Nº 11.

The elements deformations will not exceed 2/3 times of those for which they would lose their bearing capacity under vertical loads or for those that will get a strength reduction of more than 30 %.

To verify the element strength, the analysis result will be divided by $R = 2$, using the standards applicable for each material.

CHAPTER 5 STIFFNESS, STRENGTH AND DUCTILITY REQUIREMENTS

5.1 Determination of Lateral Displacements

For regular structures, the lateral displacements will be calculated multiplying by 0,75 *R* the result obtained from the lineal and elastic analysis with the reduced seismic stresses. For irregular structure, the lateral displacement will be calculated by multiplying by 0,85 *R* the result obtained from the linear elastic analysis.

For the calculation of lateral displacement, the minimum *C*/*R* indicated in the item 4.5.2 and the minimum base shear specified in the item 4.6.4 won't be considered.

5.2 Permissible Lateral Displacements

The maximum relative story displacement, calculated according to item 5.1, should not exceed the fraction of the story height (Drift) indicated in Table N° 11.

Note: The limits of distortion (Drift) for structures of industrial use will be established by the designer, but in no case they will exceed twice the values of this Table.

5.3 Seismic Separation Joints between Buildings (*s***)**

Every structure should be separated from other close structure, from the level of natural area, a minimum distance *s* to avoid the contact during an earthquake

This distance will not be lower than 2/3 of the sum of maximum displacements of the adjacent building, nor lower than:

s = 0,006 *h* ≥ 0,03 m

Where *h* is the height measure from the level of natural area to the level considered to evaluate *s*.

The building will be moved away from the adjacent properties, the distances will not less than 2/3 of the maximum displacement calculated according to item 5.1 nor less than *s*/2 if the existing building has a regulatory seismic joint. In the case that there is no regulatory seismic joint, the building should be separated from the existing building the value of *s*/2 that corresponds plus the value s/2 of the neighboring structure

5.4 Redundancy

When there is an element in the structure, wall or frame, where the force is 30% or more of the total horizontal base shear force acting in any inter story, the element shall be designed for 125% of that force.

5.5 Verification of the Ultimate Resistance

In case there is realized an analysis of the Ultimate Resistance it will be use the specification of the ASCE/SEI 41 SEISMIC REHABILITATION OF EXISTING BUILDINGS. This disposition does not constitute a requirement of this Standard.

CHAPTER 6 NON-STRUCTURAL ELEMETS, APENDIXES AND EQUIPMENT

6.1 Overview

Nonstructural elements are those that, whether connected or not to the system resistant to horizontal forces, contribute mass to the system but their contribution of the rigidity is not significant

For non-structural elements that are joined to the earthquake resistance structural system and should accompany the deformation of the structure, it must be ensured that in case of fault they should not cause damage

Within the nonstructural elements that must have adequate resistance and rigidity for seismic action they included.

- Fences, partitions, parapets, prefabricated panels.
- Architectural and decorative elements between ceilings veneers.
- Glasses and curtain wall
- Hydraulic and sanitary installations
- Electrical installations
- Gas installations.
- Mechanical equipment
- Furniture whose instability means a risk

6.2 Professional Responsibility

The professional who elaborate the different projects will be responsible for providing the nonstructural elements with adequate resistance and rigidity for seismic action

6.3 Forces of Design

Nonstructural elements, the anchor, and connection will have to be designed to resistance a seismic horizontal force in any direction (*F*) associated to his weight (*Pe*), whose resultant one be able to be supposed applied in the center of masses of the element, as indicated then.

$$
F = \frac{a_i}{g} \cdot C_1 \cdot P_e
$$

Where *aⁱ* is the horizontal acceleration at the level where the nonstructural element is supported, or anchored, to the structural system of the building. This acceleration depends on the dynamic characteristic of the structural system of the building and must be evaluated by means of a dynamic analysis of the structure.

Alternatively the following equation can be used:

$$
F = \frac{F_i}{P_i} \cdot C_1 \cdot P_e
$$

Where *Fⁱ* is the lateral force in the level where the nonstructural element is calculated according to the numeral 4.5 and P_i the weight of the above mentioned level.

The values of C_1 will be taken from Table N° 12.

To calculate the forces of design on wall, partitions and in general nonstructural elements design with distributed mas, the force F will be taken a distributed load uniform by a unit area. For wall and partitions supported horizontally in two consecutive levels, the average of the acceleration of the two levels will be taken.

6.4 Mínimum Horizontal Force

In no level of the building the force *F* calculated with the item 6.3 will be less than $0.5 \cdot Z \cdot U \cdot S \cdot P_e$.

6.5 Vertical Seismic Forces

The seismic vertical force will be considered to be 2/3 times the horizontal stress.

For equipment supported by elements of big lights elements, including floats, a dynamic analysis shall be required with the spectra defined in the item 4.6.2.

6.6 Non Structural Elements Located on Base of Structure, Under Base and Fences

Nonstructural elements located at or below the base of the structure (Basement) and fences shall be designed with horizontal force calculated with:

$$
F=0,5\cdot Z\cdot U\cdot S\cdot P_e
$$

6.7 Other Structures

For Signs, chimneys, tower and communication antennas installed at any level of the building, the design strength will be established considering the dynamic properties of the building and the structure it be installed. The design strength should not be less than the correspondent to the calculated one with the methodology proposed in this chapter with a minimum value of C_1 of 3,0.

6.8 Design using the Method of Admissible Stresses

When a nonstructural element or the anchor are designed using the Method of Admissible Stresses, the seismic forces defined in this chapter shall be multiplying by 0,8.

CHAPTER 7 FOUNDATIONS

7.1 Overview

The structure support assumptions must be in accordance with the foundation subsoil characteristics.

The applied pressure on soil used in the Allowable Strength Design (ASD) must be determined using the forces obtained from the seismic analysis factored by 0.8.

7.2 Bearing Capacity

Every Geotechnical study must consider the effects of earthquake to obtain the bearing capacity of soil foundations. In case of soil prones to liquefaction, the geotechnical prospection and geotechnical study must evaluate the liquefaction potential and the proper solution.

7.3 Overturning Moment

Both the superstructure and foundation must be designed against seismic overturning moment following items 4.5 or 4.6. The safety factor of forces result of the application of this Manual must be greater than or equal to 1.2.

7.4 Foundations on soft or low bearing capacity soils

Isolated foundation and piles into soils type S_3 y S_4 located in Zone 4 and 3 must have connection elements between them, which must bear in traction and compression, a minimum horizontal load equal to 10% the applied vertical load to foundation.

Beam foundations in both directions must be provided in case of soils of bearing capacity less than 0,15 MPa.

In case of piles and caisson beam fundations must be used or, piles and isolated foundations must be designed taken in account rotation and deformation caused by the horizontal force. Piles must have a tensile steel reinforcement equal to at least 15% the bearing vertical load.

CHAPTER 8 EVALUATION, REHABILITATION AND RETROFITTING OF STRUCTURES

The damage structures by earthquakes shall be evaluated, rehabilitated or retrofitted in order to correct structural defects and recovery the capacity to resist a new seismic event, following the seismic design philosophy specified in Chapter 1.

8.1 Evaluation of structures after an earthquake

After a seismic event, the structure shall be evaluated by a civil engineer, who should decide if the structure is in good condition or need retrofitting, strengthening or demolition. The study shall consider geotechnical characteristics of site.

8.2 Rehabilitation and retrofitting

The rehabilitation or retrofitting shall provide adequate combination of stiffness, resistance and ductility to the structure to improve the behavior due earthquakes.

The rehabilitation or retrofitting project will include the details, procedures and constructive system to follow.

The seismic rehabilitation and retrofitting of structures follow guidelines of National Building Regulation (RNE). Only in exceptional cases may be used other criteria or procedures different to RNE, with technical justification and approval of the owner and the competent authority.

Essential buildings may be intervene using the criteria of incremental seismic retrofit and to extent applicable, using established criteria in the guideline "Engineering Guideline for Incremental Rehabilitation", FEMA P-420, Risk Management Series, USA 2009.

CHAPTER 9 INSTRUMENTATION

9.1 Accelerometric Stations

An accelerometer station is a secure space with sufficient area, housing a triaxial acceleration sensor, a signal recording, storage, and transmission system from the recording point to the processing center. The station must have suitable conditions for accurately recording seismic vibrations, with controlled timing, and stable and secure electrical power.

The accelerometer stations are provided by the owner and must comply with the technical specifications set by the Geophysical Institute of Peru (IGP), according to the document "Technical Specifications for Accelerometric Recorders and Minimum Requirements for their Installation, Operation, and Maintenance."

Buildings that, individually or collectively, have a roofed area equal to or greater than 10,000 m2, must have an accelerometer station installed at ground level or at the base of the building.

For buildings with more than 20 floors or those equipped with seismic dissipation or base isolation devices, regardless of their height, an additional accelerometer station is required. This station should be installed at the roof or at the level immediately below the roof in addition to the one at the base.

The implementation of what is established in this section is part of the other operational facilities of the common assets and services on the habitable core level of the building.

9.2 Location requirements

The accelerometric station shall be install at a suitable area, with easy access for maintenance and proper illumination, ventilation, stabilized power supply.

The area shall be away from sources that generate any type of anthropic noise.

The instrumentation plan shall prepare by designers of each specialty and clearly indicated in the architectural, structures and installation planes of the building.

9.3 Maintenance

The operational maintenance of the parts, components consumables, service of instruments, shall be provided by the buildings/department owner, under municipality control and shall be supervised by the IGP. Responsibility owner will be maintained for 10 years.

9.4 Data availability

Recorded information by the instruments will be integrated to the National Geophysical Data Center and will be available to the public.
APPENDIX Nº **1 SUGGESTED PROCEDURE FOR THE DETERMINATION OF SEISMIC ACTIONS**

Seismic actions for structural design depend on the seismic zone (*Z*), soil profile (*S*, *TP*, *TL*), building usage (*U*), seismic-resistant system (*R*), dynamic characteristics of the building (*T, C*), and its weight (*P*).

STAGE 1: SEISMIC HAZARD (Chapter II)

The steps in this stage depend solely on the location and characteristics of the project's foundation terrain. They are not influenced by the building's characteristics.

Step 1: Zone Factor Z (section 2.1)

Determine the seismic zone where the project is located based on the seismic zoning map (Figure No. 1) or the Table of provinces and districts in APPENDIX N°02. Determine the zone factor (*Z*) according to Table No. 1.

Step 2: Soil Profile (section 2.3)

Based on the results of the Soil Mechanics Study (SMS), determine the type of soil profile according to section 2.3.1, which defines 5 soil profiles. The classification is based on parameters indicated in Table No. 2, considering averages for the strata within the first 30 m below the foundation level. When soil properties are not known to a depth of 30 m, the professional responsible for the SMS determines the soil profile type based on known geotechnical conditions.

Step 3: Site Parameters S, TP, and TL (section 2.4)

The soil amplification factor is obtained from Table No. 3 and depends on the seismic zone and the type of soil profile. The periods T_P and T_L are obtained from Table No. 4 and depend solely on the type of soil profile.

Step 4: Construct the Seismic Amplification Factor C versus Period T Function (section 2.5)

It depends on the site parameters T_P and T_L . Three ranges are defined: short, intermediate, and long periods, and the expressions in this section are applied to each range.

STAGE 2: BUILDING CHARACTERIZATION (Chapter III)

The steps in this stage depend on the characteristics of the building, such as its category, structural system, and regular or irregular configuration.

Step 5: Building Category and Usage Factor U (section 3.1)

The building category and the usage factor (*U*) are obtained from Table No. 5.

Step 6: Structural System (sections 3.2 and 3.3)

Determine the structural system according to the definitions in section 3.2. Table No. 6 (section 3.3) defines the allowed structural systems based on the building category and the seismic zone in which it is located.

Step 7: Basic Seismic Force Reduction Coefficient, *R⁰* **(section 3.4)**

Obtain the value of the coefficient *R⁰* from Table No. 7, which depends solely on the structural system.

Step 8: Irregularity Factors *Ia***,** *I^p* **(section 3.6)**

The factor *I^a* is determined as the minimum of the values in Table No. 8 corresponding to height irregularities. The factor I_p is determined as the minimum of the values in Table No. 9 corresponding to plan irregularities. In most cases, it can be determined whether a structure is regular or irregular based on its structural configuration. However, in cases of Stiffness Irregularity and Torsional Irregularity, it is verified with the results of the seismic analysis as indicated in the description of these irregularities.

Step 9: Irregularity Constraints (section 3.7)

Verify the irregularity constraints according to the building category and zone in Table No. 10. Modify the structure if the constraints in this table are not met.

Step 10: Seismic Force Reduction Coefficient R (section 3.8)

Determine $R = R_0 \cdot I_a \cdot I_p$

STAGE 3: STRUCTURAL ANALYSIS (Chapter IV)

In this stage, the structural analysis is carried out. Criteria for developing the mathematical model of the structure are suggested, the calculation of the building's weight is outlined, and analysis procedures are defined.

Step 11: Analysis Models (section 4.2)

Develop the mathematical model of the structure. For reinforced concrete and masonry structures, consider the properties of gross sections, ignoring cracking and reinforcement.

Step 12: Estimation of Weight P (section 4.3)

Determine the weight (*P*) for the seismic force calculation by adding to the total permanent load a percentage of the live load, which depends on the usage and category of the building, as defined according to the information in this section.

Step 13: Seismic Analysis Procedures (section 4.4 to 4.7)

The analysis procedures considered in this Standard are defined, which include static analysis (section 4.5) and modal spectral dynamic analysis (section 4.8).

Step 13A: Static Analysis (section 4.5)

This procedure is only applicable to structures that meet the requirements stated in section 4.5.1. The static analysis involves the following steps:

- Calculate the base shear $V = \frac{Z \cdot U \cdot C \cdot S}{R}$ \overline{R} *⋅ P* for each direction of analysis (section 4.5.2).
- To determine the value of *C* (Step 4 or section 2.5), estimate the fundamental vibration period of the structure (*T*) in each direction (section 4.5.4).
- Determine the distribution of seismic force over the height for each direction (section 4.5.3).
- Apply the obtained forces at the center of mass of each floor. Additionally, consider accidental torsional moments (section 4.5.5).
- Consider vertical seismic forces (section 4.5.6) for elements where necessary.

Step 13B: Dynamic Analysis (section 4.6)

If choosing or required to conduct a modal spectral dynamic analysis, the following steps should be taken:

- Determine the modes of vibration and their corresponding natural periods and participating masses through dynamic analysis of the mathematical model (section 4.6.1).
- Calculate the inelastic spectrum of pseudo-accelerations $S_a = \frac{Z \cdot U \cdot C \cdot S}{R}$ *R*^{*R*} *c g* for each analysis direction (section 4.6.2).
- Consider accidental eccentricity (section 4.6.5).
- Determine all force and displacement results for each mode of vibration.
- Determine the maximum expected response corresponding to the combined effect of the considered modes (section 4.6.3).
- Scale all force results (section 4.6.4) considering a minimum shear at the first floor that is a percentage of the shear calculated for the static method (section 4.6.3). Do not scale displacement results.
- Consider vertical seismic forces (section 4.6.2) using a spectrum with values equal to 2/3 of the most critical spectrum for horizontal directions, for elements where necessary.

STAGE 4: STRUCTURAL VALIDATION

Based on the analysis results, it is determined whether the proposed structure is valid, ensuring that it complies with the regularity and stiffness requirements outlined in this chapter.

Step 14: Review of Analysis Assumptions

With the results of the analyses, review the irregularity factors applied in step 8. Based on these, verify whether the values of *R* remain unchanged or are modified. In the case of using the static analysis procedure, verify what is indicated in section 4.5.1.

Step 15: Irregularity Constraints (section 3.7)

Verify the irregularity constraints according to the building category and zone in Table No. 10. If there are irregularities or extreme irregularities in buildings where they are not allowed according to that table, modify the structure and repeat the analysis until a satisfactory result is achieved.

Step 16: Determination of Lateral Displacements (section 5.1)

Calculate the lateral displacements according to the instructions in this section.

Step 17: Allowable Distortion (section 5.2)

Verify that the maximum interstory drift obtained in the structure with the calculated displacements from the previous step is less than the values indicated in Table No. 11. If not satisfied, review the structure and repeat the analysis until the requirement is met.

Step 18: Building Separation (section 5.3)

Determine the minimum separation to other buildings or the property boundary according to the instructions in this section.

APPENDIX Nº **2 SEISMIC ZONATION**

The seismic zones in wich the Peruvian territory is divided, for the puspose of this standartd are shown in Figure 1

The provinces of each area are specified as follows:

